

Review paper

Stoop or squat: a review of biomechanical studies on lifting technique

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Abstract

Objective. To assess the biomechanical evidence in support of advocating the squat lifting technique as an administrative control to prevent low back pain.

Background. Instruction with respect to lifting technique is commonly employed to prevent low back pain. The squat technique is the most widely advised lifting technique. Intervention studies failed to show health effects of this approach and consequently the rationale behind the advised lifting techniques has been questioned.

Methods. Biomechanical studies comparing the stoop and squat technique were systematically reviewed. The dependent variables used in these studies and the methods by which these were measured or estimated were ranked for validity as indicators of low back load.

Results. Spinal compression as indicated by intra-discal pressure and spinal shrinkage appeared not significantly different between both lifting techniques. Net moments and compression forces based on model estimates were found to be equal or somewhat higher in squat than in stoop lifting. Only when the load could be lifted from a position in between the feet did squat lifting cause lower net moments, although the studies reporting this finding had a marginal validity. Shear force and bending moments acting on the spine appeared lower in squat lifting. Net moments and compression forces during lifting reach magnitudes, that can probably cause injury, whereas shear forces and bending moments remained below injury threshold in both techniques.

Conclusion. The biomechanical literature does not provide support for advocating the squat technique as a means of preventing low back pain.

Relevance

Training in lifting technique is widely used in primary and secondary prevention of low back pain, though health effects have not been proven. The present review assesses the biomechanical evidence supporting the most widely advocated lifting technique. © 1999 Elsevier Science Ltd. All rights reserved.

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1. Introduction

In view of the high costs associated with low back pain (LBP) and the high recurrence rate of the complaints, primary prevention has received considerable interest. Several recent review studies on the epidemiology of LBP conclude that lifting is the best documented risk factor for this disorder [1–4]. In line with this, preventive strategies often involve measures aimed at reducing back load associated with lifting tasks. Next to engineering controls, administrative controls such as training and instruction in particular with respect to

lifting technique are widely used [5–11]. Intervention studies have failed to demonstrate convincing effects of training and instruction with respect to lifting technique on musculoskeletal health. Health effects of training programmes with respect to lifting technique were either lacking or minimal [5,8,12–17]. This may be due to a lack of skill or willingness of workers to apply the lifting techniques taught [5,9,10,18], but also the rationale behind the principles taught has been questioned [9].

The most commonly advised lifting technique is the so-called squat technique or leg lift, in which the back remains as erect as possible and in which the knees are flexed [19]. It can easily be understood that compliance with this advise is often low, given the high energetic

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cost of this technique [20–22], causing higher perceived exertion and more rapid fatigue development [23,24], as compared to its exact opposite the stoop technique. In repetitive lifting experiments, subjects have been shown to shift from a squat technique to a stoop technique, probably to avoid or diminish fatigue development [25–28]. Better training programmes can possibly overcome this low compliance. However, if the rationale behind promoting the squat technique is dubious, more effort in improving methods of training and instruction does not seem warranted. The aim of the present review therefore was to evaluate the evidence that the lifting technique is an important determinant of the probability of contracting LBP. Since the premise behind training in lifting technique is that the mechanical load during lifting determines this probability, biomechanical studies on lifting technique were reviewed. This review was limited to studies comparing the stoop and squat techniques, as these are well defined and frequently studied techniques in manual materials handling. In addition, a limitation is made to symmetric lifting, since all the available data suggests that symmetric lifting is to be preferred over asymmetric lifting [29–35].

2. Methods

2.1. Literature search

This review was based on a literature search in the following databases: Medline, Current Contents, Embase, and NIOSHTIC, using the keywords lifting and technique. These references were screened on the basis of titles and abstracts and those papers concerning a biomechanical evaluation of lifting techniques were selected for further study. The literature retrieved in this way was supplemented with references from reviews with a somewhat broader scope [36–38] and studies cited in the previously retrieved papers.

2.2. Selection and evaluation of validity of dependent variables

It is unknown what structures are responsible for LBP, and it seems likely that different structures may be involved in different cases. Therefore, all mechanical loads likely to induce injury to structures in the low back will be considered, this includes loads on spinal structures (e.g., ligaments, intervertebral disc, vertebrae) and musculotendinous structures (e.g., muscle, musculotendinous junction, tendinous insertion).

The mechanical load on the osteoligamentous spine during symmetric lifting consist of three components, each of which according to *in vitro* studies has the potential to cause injury. High compression forces are caused mainly through back muscle activity. These may

cause the vertebral endplate to fracture and the intervertebral disc to prolapse into the vertebra [39,40]. Considerable forward shear forces can occur, as a result of gravity acting on the upper body and of muscular forces. These shear forces can cause damage to the neural arch [41,42] and possibly to the facet joints. Finally, bending of the trunk imposes tensile stresses on the posterior spinal ligaments and the posterior intervertebral disc, which can cause damage to these structures [43,44]. Muscular damage is most likely to occur when high forces are sustained or produced repeatedly. Eccentric contractions are especially likely to cause muscular damage, but this type of damage appears to be reversible within days [45,46] and is somewhat outside the scope of this review. In conclusion, four parameters appear of interest: compression and shear acting on the spine, tensile stresses in the posterior spine, and muscle force. Note that these parameters are not independent. For example, the compression forces on the lumbar spine are determined mainly by muscle forces.

Unfortunately, none of the four variables of interest can be measured directly. Therefore, indicators of these parameters of back load have been used, some based on measurements, some on model calculations (summarised in Table 1). The validity of these indicators will be evaluated in the following and a score for validity of each indicator and estimation method will be given. This score will be used in weighing the results of different studies. Invalid indicators will be given a score 0 and will be excluded from the review. Measured and highly valid indicators of back load will get a score of 3, model-based sufficiently validated estimates will get a score of 2 and indicators with a limited validity will get a score of 1. Findings based on the latter category will be considered valid, only in case the results converge with evidence based on more valid indicators.

In general, measurements are to be preferred over model calculations in view of the assumptions involved in modelling. However, the possibilities for measurements of the load on the low back are, as stated above, very limited. The measurements that have been applied in studying lifting techniques are intra-discal pressure (IDP), intra-abdominal pressure (IAP), spinal shrinkage, and EMG.

IDP measurements can be considered the most direct indicator of compression forces acting on the spine [47,48]. These measurements are generally considered highly valid indicators of spinal compression, but the invasive nature limits their applicability. Consequently, only few data are available.

IAP has been suggested to be an indicator of spinal compression [49]. However, IAP increase has also been suggested to be a means of relieving the spine from high compression forces [50,51]. In addition to this inconsistency, the relationship between IAP and IDP appears to be disturbed by trunk posture [52–54]. Therefore,

Table 1

Parameters of back load and their indicators derived from direct measurements or model calculations evaluated for use in comparative studies of lifting technique

Parameter of back load	Indicator	Method	Evaluation ^a	Comments
<i>Measured indicators</i>				
Muscle force	EMG	Surface EMG	0	Low validity
Compression	IDP	Invasive, pressure transducer	3	
	IAP	Radio-pill catheter	0	Inconsistent theory, low validity
Shear	Shrinkage	Stadiometry	1	Low repeatability
	None			
Bending moment + ligament stress	None			
<i>Model based estimates</i>				
Muscle force	Net moment	Static LSM	1	
		Dynamic LSM	2	
	Estimated extensor moment	Surface EMG, kinematics, muscle length and shortening velocity correction	2	
Compression + shear	Estimated compression + estimated shear	Net moment, surface EMG	2	Depends on anatomical fidelity
		Net moment, optimisation	2	Depends on anatomical fidelity
		Net moment, SEM (constant moment arm)	0 ^b	Little information additional to net moment
Bending moment + ligament stress	Estimated ligament stress, estimated bending moment	Cadaver data, trunk kinematics, force-deformation relationship	2	

^a 0 = Will be discarded, 1 = will be used in case of converging evidence, 2 = sufficiently valid for comparative use, 3 = valid indicator of back load.

^b Used only if net moments not reported, ranking in these cases according to validity of estimate of net moment.

data on IAP will not be accepted as an indicator of back load in this review.

Spinal shrinkage measurements are also considered to be indicators of compressive back loading. If applied in a repeated measures design and given certain methodological criteria, such as exclusion of the influence of prior loading, spinal shrinkage appears to be a valid indicator of spinal compression for use in comparative studies [55]. However, the repeatability of spinal shrinkage measurements is low [55,56]. Therefore, an absence of effects of lifting technique might be due to a lack of statistical power. Converging evidence from several studies will be needed to draw conclusions with sufficient confidence.

Surface EMG measurements on the back muscles have been used as indicators of back muscle force in a range of studies. Whereas the EMG amplitude appears to be a valid indicator of muscle activation, it is not necessarily a valid indicator of back muscle force [57–59]. Only when combined in a model using information on muscle length and shortening velocity relating the EMG data to calibration data on an individual level can valid estimates of back muscle force in dynamic lifting tasks be attained. Therefore, the use of EMG will be dealt with below in discussing EMG based models of low back load.

Model based indicators of low back load include net moments, estimated muscle forces or muscle moments, estimated compression and shear forces and predicted bending moments resisted by the osteoligamentous spine or tensile forces in individual ligaments.

Neglecting passive tissue contributions, the peak net moment in a lifting task reflects the peak back muscle force minimally (i.e., neglecting antagonistic coactivation) required and as such also the major component of the compression force acting on the spine [60]. Actual muscle forces and compression forces are not completely determined by the net moment though, since the distribution of the net moment across muscles and levels of cocontraction may vary. Net moments can be calculated reliably through a linked segment model (LSM) [61,62]. Some LSMs neglect accelerations of body segments, which can produce substantial errors [63–65]. Since this review deals with a comparative analysis, the results of such static models will not be discarded. However, since systematic differences in the dynamic component of the moment about the lumbar spine might exist between the squat and stoop technique, static estimates of the differences in net moments will be considered sufficient evidence only in the case of convergence with dynamic estimates. In addition, the net moment can be estimated using EMG data and a model incorporating kinematic

Table 2
Overview of particulars and main results of the included studies.^a

Study	Nr.	Dependent variable	Method	Validity	Subjects	Load	Horizontal position	Stoop	Squat	Diff. % stoop	p-Value	Conclusion	Comments	
Andersson et al. (1976)	52	IDP (Mpa)	Direct	3	3 f, 1 m	40	Fixed in front of feet				NS	=	Static pull	
Dieën et al. (1994)	74	IDP (Mpa)	Direct	3	3 f, 1 m	10	?	1.83	1.5	18	NS	=	Dynamic lift	
		Spinal shrinkage (mm)	Direct	1	11 m	8	25 vs. 30	3.9	4		NS	=	Horizontal position freely chosen	
Rabinowitz et al. (1998)	75	Spinal shrinkage (mm)	Direct	1	10 m	20% bm	Fixed in front of feet	4.12	4.81		NS	=		
Park & Chaffin (1974)	76	Net moment (Nm)	Static LSM	1	–	0–16	37.5	81	8.8	–9	–	–	Model study	
		Net moment (Nm)	Static LSM	1	–	0–16	50	100	111	–11	–	--		
		Net moment (Nm)	Static LSM	1	–	0–8	75	105	103	103	2	–	=	
		Net moment (Nm)	Static LSM	1	–	0–70	31 vs. 12	256	226	226	12	–	++	Model study
Garg & Herrin (1979)	20	Net moment (Nm)	Static LSM	1	–	0–50	38	238	246	–3	–	=		
		Net moment (Nm)	Static LSM	1	14 m, 1 f	12.8	Variable, close	217	160	26	<0.001	++		
Ekholm et al. (1982)	77	Net moment (Nm)	Static LSM	1	14 m, 1 f	12.8	Variable, far	217	200	8	NS	=		
		Net moment (Nm)	Static LSM	1	5 m	25	Variable	182	120	34	<0.0.01	++		
Wax et al. (1987)	78	Net moment (Nm)	Static LSM	1	10 m	12.8	30	186	167	10	<0.01	++	Load between feet in squat	
Lindbeck & Arborelius (1991)	79	Net moment (Nm)	Static LSM	1	100 f	18 vs. 17	Variable	295	250	15	<0.05	++	Loads differed between techniques, static holding	
Mittal & Malik (1991)	80	Net moment (Nm)	Static LSM	1	100 f	18 vs. 17	Variable	295	250	15	<0.05	++		
Looze et al. (1992)	64	Net moment (Nm)	Static LSM	1	5 m	11	40 ^b	184	185	–1	NS	=		
Bush-Joseph et al. (1988)	81	Net moment (Nm)	Dynamic LSM	2	10 m	15	38			–18	<0.05	--		
Buseck et al. (1988)	82	Net moment (Nm)	Dynamic LSM	2	10 m	5–25	37	309	268	13	?	?	Stoop = free technique, performed faster	

(continued overleaf)

Table 2 (continued)

Study	Nr.	Dependent variable	Method	Validity	Subjects	Load	Horizontal position	Stoop	Squat	Diff. % stoop	p-Value	Conclusion	Comments
Potvin et al. (1991)	83	Net moment (Nm)	Dynamic LSM	2	15 m	6–32	?	290	277	4	?	?	
Lindbeck & Arborelius (1991)	79	Net moment (Nm)	Dynamic LSM	2	10 m	13	30	268	290	-8	NS	=	
Looze et al. (1992)	64	Net moment (Nm)	Dynamic LSM	2	5 m	11	40 ^b	265	255	4	NS	=	
Toussaint et al. (1992)	85	Net moment (Nm)	Dynamic LSM	2	8 m	15	Fixed in front of feet	225 ^b	225 ^b	0	NS	=	
Hagen & Harms-Ringdahl (1994)	86	Net moment (Nm)	Semi-dynamic LSM	2	10 m	1–17	Fixed in front of feet	200 ^b	193 ^b	0	NS	=	
Dolan et al. (1994a)	87	Extensor moment (Nm)	EMG based	2	23 m, 126 f	10	?	243	252	-4	<0.05	-	
Dolan et al. (1994b)	88	Extensor moment (Nm)	EMG based	2	21 m, 18 f	0–30	?	228	254	-11	<0.0001	--	
Dieën et al. (1994)	74	Net moment (Nm)	Dynamic LSM	2	11 m	8	25 vs. 30	196	214	-9	0.04	-	Horizontal position freely choosen
Toussaint et al. (1997)	89	Net moment (Nm)	Dynamic LSM	2	8 m	20% BM	51.5 ^b	368	366	1	NS	=	
Kjellberg et al. (1998)	94	Net moment (Nm)	Dynamic LSM	2	12 f	8.7	50 ^b	150	151	-1	NS	=	
Looze et al. (1998)	90	Net moment (Nm)	Dynamic LSM	2	8 m	7–16	38 ^b	210	228	-9	<0.001	--	
Troup et al. (1983)	91	Compression (N)	Dynamic LSM + SEM	2	10 m	15	In front of feet	5767	6039	-5	<0.001	-	Feet placed asymmetrically in squat
Leskinen et al. (1983)	92	Compression (N)	Dynamic LSM + SEM	2	20 m	15	Fixed feet under load	6365	5866	8	<0.01	+	
Leskinen et al. (1985)	63	Compression (N)	Static LSM + SEM	1	20 m	15	Fixed feet under load	3989	4033	-1	NS	?	
Anderson & Chaffin (1986)	73	Compression (N)	Static LSM + opt.	1	1	5–40	Between legs	5055	3304 ^c	35	-	++	Crude anatomical model
Potvin et al. (1991)	83	Compression (N)	Static LSM + opt.	1	1	5–40	In front of feet	3931	4275 ^c	-9	-	-	Partly predicted kinematics
Potvin et al. (1992)	84	Compression (N)	Dynamic LSM + EMG	2	15 m	15	?	4275	4724	-11	<0.05	--	
Potvin et al. (1992)	84	Compression (N)	Dynamic LSM + EMG	2	13 m	6–32	34 vs. 32			-6 ^b	0.02	-	

(continued on next page)

Table 2 (continued)

Study	Nr.	Dependent variable	Method	Validity	Subjects	Load	Horizontal position	Stoop	Squat	Diff. % stoop	p-Value	Conclusion	Comments
Chaffin & Page (1994)	93	Mass at 3400N comp. (Kg)	Static LSM + opt.	1	–	Dep. var.	38–58	16 ^b	10 ^b	–	–	–	Model study, predicted kinematics
Potvin et al. (1991)	83	Shear (N)	Dynamic LSM + EMG	2	15 m	15	?	450	156	65	<0.05	++	
Anderson & Chaffin (1986)	73	Fascial strain (%)	Kinematics based	2	1	5–40	Between legs	3.6	2.3 ^c	36	–	++	Partly predicted kinematics
		Fascial strain (%)	Kinematics based	2	1	5–40	In front of feet	8.8	2.4 ^c	73	–	++	Partly predicted kinematics
Dolan et al. (1994a)	87	Bending moment (Nm)	Kinematics based	2	23 m, 126 f	10	?	75	54	28	<0.05	++	
Dolan et al. (1994b)	88	Bending moment (% max)	Kinematics based	2	21 m, 18 f	0–30	?	31	18	42	<0.05	++	

^a m – male; f – female; – – – substantial (>10%) negative effect of squat technique; – is limited (<10%) negative effect of squat technique; = – no effect of lifting technique; + – limited (<10%) positive effect of squat technique; ++ – substantial (>10%) positive effect of squat technique.

^b Estimated.

^c Curved back squat and flat back squat averaged.

data [66]. Comparisons to the outcomes of LSMs indicate this to be a valid method [67,68].

Muscle forces can be estimated from the net moment using optimisation, EMG, or using a single-equivalent muscle model (SEM). The latter adds little to the information contained in the net moment and will be discarded. The former techniques have been used in studying lifting techniques but only with the aim of predicting forces acting on the spine. Estimated muscle forces were not compared between the two techniques.

Using net moments as a starting point, forces acting on the spine can be calculated using a model of the trunk musculature. It has been shown that these estimates heavily depend on the anatomical fidelity of the model [69–71]. Major factors in this respect are the changes with trunk flexion of the moment arms of the muscles [72] and of the orientation of the muscles with respect to the spine [71]. These factors have been neglected in all SEMs applied to date. The results from such models will therefore be discarded, but the net moments from these studies when reported or when these can be calculated from the data provided will be included in the review. If the net moments cannot be derived from these papers, the reported compression forces will be considered along with the results from papers reporting net moments, since compression forces estimated with a SEM are strongly determined by the net moment. The studies using more sophisticated models to estimate compression forces apply either EMG or optimisation to obtain muscle force and finally the forces on the spine. Both methods involve a number of assumptions, which have not been sufficiently validated. A ranking of the validity of the two approaches can therefore not be made. The anatomical fidelity of the models applied will be qualitatively evaluated.

Spinal bending moments or ligament and disc stresses are estimated from trunk kinematics using models based on cadaver data. This involves a generalisation of the force-deformation relationships of the structures studied in vitro to the in vivo situation. In a comparative analysis this does not seem to be a major problem. However, the assumed deterministic relationship between trunk kinematics measured externally and internal kinematics of the spine may limit the validity.

3. Results

In total 27 studies comparing stoop and squat lifting with respect to the mechanical load on the back were included in this review [20,52,63,64,73–94], some reported on several dependent biomechanical variables. The main particulars and findings of these studies have been listed in Table 2. In the majority model-based dependent variables, in particular the net moment, were used. In only four studies measured indicators were

used, of which in one study IAP was used exclusively [91]. In three studies the compression force was estimated on the basis of a SEM, while the net moments were not reported. The results of these studies will be considered along with those studies reporting net moments. Only four studies reported estimates of compression force based on more sophisticated models and only one reported shear forces. Finally, three studies considered ligament stresses or spinal bending moments.

In several studies the comparison of the techniques was confounded with other variables. The horizontal distance often varied with technique, but this can be considered part and parcel of the technique. In one study the mass lifted varied with technique [80]. However, since the effect of lifting technique was a 15% change in the estimated net moment and the load mass differed by only 5%, the conclusions of this study appear to hold at least qualitatively. In some studies the velocity of lifting was reported to be higher in squat lifting as compared to stoop lifting [74,82]. Since net moments increase with lifting velocity [64,81,82], this may confound the comparison of techniques. This may have occurred in more studies, since velocity was usually not strictly controlled. However, since this occurred even when subjects were instructed to lift at a fixed pace [74], this can again be considered an integral part of the lifting technique. Therefore, no studies were excluded because of confounding of lifting technique with velocity of lifting. One study reported an opposite effect of technique on velocity, but in this study the squat technique was actually compared to a freely chosen technique [81].

The three studies in which sufficiently valid measured indicators of back load were used have been listed in the top rows of Table 2. IDP was measured in just one study involving only four subjects. No significant effect of lifting technique was found. The two studies employing spinal shrinkage measurements also failed to show any difference between stoop and squat lifting. In conclusion, measured indicators of low back load do not provide evidence, supporting preference of one lifting technique to the other. It must be kept in mind that a lack of statistical power may underlie these findings.

The seven studies using a static LSM to estimate the net moment yielded varying results. The majority of studies ($n=5$) predicted a substantial reduction (10–34%) in back load when using the squat technique in at least one of the experimental conditions. This may, however, be explained by differences in the horizontal position of the load. This issue was specifically addressed in two of these studies [20,77], which showed that when horizontal distance is constant the effect of technique disappears. The large positive effects associated with squat lifting in some of these studies can, in line with this, be explained by the fact that the load is

lifted from a position between the feet. The thirteen studies in which the net moment or extensor moment was estimated using dynamic analysis techniques found back loads in the two techniques to be either significantly higher (4–18%) in squat lifting or not significantly different. In ten of these studies, the loads were lifted from a position in front of the feet. In three studies the horizontal position of the load was not described, nor could it be derived from any of the figures. Two studies did not report whether the differences found were significant. One of these did report a substantially lower (13%) net moment in squat lifting. However, in this study subjects were not instructed with respect to the stoop technique and so actually used a free technique, which is usually intermediate between squat and stoop lifting [95]. In addition they performed this technique at a substantially higher velocity, which will strongly increase the net moment [64,81,82]. The three studies providing compression force estimates based on a SEM did yield disparate results. Leskinen analysed the same data in two papers, dynamically and statically [63,92]. The dynamic analysis yielded significantly lower compression estimates for squat lifting. In the static analysis no significant difference was found. Troup et al. [91], using the same model, found higher compression estimates for squat lifting. Again differences in load placement may explain these discrepancies. In the study by Leskinen et al. [92] subjects placed the feet below the load. As outlined in the methods section, these studies cannot actually be considered to yield a valid prediction of compression forces, but the calculation of net moments to which the compression estimates are strongly related does appear to be valid. These results will therefore be pooled with the results on net moments and extensor moments. Concluding on this complete category, the data suggest that squat lifting may be advantageous for a limited range of lifting tasks in which the load can be lifted from between the feet (up to 34% reduction in net moment). In situations where this not the case, the effect of squat lifting appears to be negative rather than positive though this effect is smaller (up to 11% increase in net moment).

In one of the studies reporting more sophisticated estimates of compression forces [73] a still fairly crude anatomical model of the lumbar spinal musculature was used [96]. Furthermore, this and one other study [93] were based on completely or partially predicted kinematics instead of experimental data and the LSM used to estimate the net moments was static. Potvin et al. [83,84] used a detailed anatomical model [97] and the net moments were calculated employing a dynamic LSM and empirical kinematic data. Overall, the results from these four studies appear in line with the above conclusions drawn on the basis of moment estimates. Given the strong relation between net moments and compression forces [84], this correspondence is not surprising.

Results on shear forces were reported in one study only [83]. As expected, shear forces were higher in stoop lifting than in squat lifting. Bending moments (and ligament stresses) were found to be substantially higher in stoop lifting than in squat lifting in all three studies reporting this variable [73,87,88].

4. Discussion

The main findings of this review were a potential positive effect of squat lifting in terms of net moments and compression forces on the spine in a limited range of lifting tasks, and no or even a limited negative effect in other lifting tasks. In terms of shear forces on the spine and tensile stresses in the posterior spinal ligaments the squat lift was found to be beneficial.

Positive effects of squat lifting with respect to estimated moments and compression forces were found only when squat lifting allowed for lifting from a position between the feet. This effect appears to entail a maximum reduction in back load by about one third. In practice, lifting from a position between the feet is often not possible and these results thus appear to be valid for a limited range of tasks. Actually in a study by Dieën et al. [74], subjects lifting a barbell preferred a larger horizontal distance when using a squat technique as compared to a stoop technique. In addition, data on lifting with the squat technique from a position between the feet based on a dynamic analysis appears to be missing. Actually the studies showing this benefit of squat lifting had a rating of 1 for the method used. Hence the validity of the positive findings on squat lifting in these cases may be questioned. A striking finding in this respect is the fact that the positive effect of squat lifting in the study by Lindbeck and Arborelius [79] disappeared, when reanalysing the same data using a dynamic LSM. The much higher ground reaction forces in squat lifting related to the greater vertical excursion of the body centre of mass [89], which are ignored in a static analysis, may account for this. However, in comparable studies this effect was not found, or the dynamic analysis predicted, in contrast to the static analysis, a positive effect of the squat technique [63,64]. Hence the results from the static analyses should not be discarded altogether.

In lifting tasks where the load is not lifted from a position between the feet, the net moment and compression tended to be lower using the stoop technique. In contrast, in all studies reporting shear and bending moments, these were higher in stoop lifting. Consequently, the parameters of back load these indicators stand for need to be weighted with respect to each other. When a parameter increases with a change in lifting technique, but remains well below injury threshold, this increase can be considered of little importance. Thus the

injury potential of the parameters of back load could be used to obtain such a weighting.

The net moments in Table 2, which, as determined using a dynamic LSM, range from about 190 to 370 Nm for male subjects, can be compared to the muscle strength, as determined in static strength tests. In several experiments we found the average maximum extension moment in healthy males to be over 300 Nm with a standard deviation of up to 30% of the mean [98–101]. Therefore, even in the healthy young male (age < 30 yr) population included in these experiments the net moments in lifting can approach the static maximum moment. In a selected group of five physically inactive young males the average maximum moment was 269 (SD 35) Nm [99], comparable to the average value of 234 Nm among 27 male industrial workers not selected for age [102]. McNeil et al. [103] reported even lower values. For inactive subjects or subjects over 30 years old, net moments during lifting can thus certainly exceed the voluntary static maximum moment. The incidence of back injuries appears to increase when this occurs in occupational lifting tasks [104,105]. In view of these findings, the effect of lifting technique on the net moment can be considered important.

Lumbar spinal motion segments fail under compression at levels in between about 2 and 10 kN [40,106,107]. Their strength appears to be age and sex dependent. Compression forces of 3–5 kN, as occur during lifting according to the studies listed in Table 2, are high enough to cause failure in females over 20 and in males over 40 years old [106] and probably in younger males under repetitive loading [108,109]. It has been hypothesised that a major proportion of all LBP cases is attributable to excessive compression during tasks such as lifting [110]. Consequently, effects of lifting technique on compression forces can be considered important. In the context of the comparison of stoop and squat lifting, it is important to note that compression strength is not significantly affected by flexion of the motion segment [111].

Shear forces on lumbar spinal motion segments were reported in one study only. Forward shear forces of up to 450 N were found. To our knowledge only two studies present strength data of human motion segments with respect to anterior shear. Cyron et al. [42], reported strength values ranging from a minimum of about 1 to a maximum of 2.5 kN. Lamy and associates [41] reported a similar minimum strength and a maximum strength of over 5 kN. This would suggest that shear forces during lifting do not pose a serious injury risk as was suggested by Cyron [42]. However, it should be kept in mind that in repetitive loading lower shear forces may cause damage [112]. In addition, shear forces estimates during lifting are strongly dependent on the functional and anatomical assumptions in the model used [71,113]. In conclusion, though the relevance of loading in anterior shear during lifting has not been shown convincingly,

reductions in shear force may prove important, when more accurate data on shear magnitude during lifting as well as on the shear strength of the spine become available.

The bending moments carried by the osteoligamentous spine during lifting can directly be compared to the maximum bending moments as was actually done in one of the studies in Table 2 [88]. This study, as well as a previous study [114], showed that bending moments during lifting remain well below the injury threshold. Consequently, the difference in bending moment between the two lifting techniques can be considered not very relevant.

In conclusion, the present review shows that there is no substantial biomechanical evidence to support training and instruction in which the squat technique is advocated. Evidence obtained with other approaches such as psychophysics and exercise physiology, generally appears to support this conclusion [20–24]. In addition, it has been shown that balance loss during lifting, which may cause excessive back load, is more likely to occur when using the squat technique as compared to the stoop technique [89]. It is, therefore, suggested that controls for preventing LBP associated with lifting should be focussed on other aspects of lifting. The most promising interventions would deal with those factors, that have been shown to substantially affect the mechanical load on the low back, such as asymmetry [29,31–33,35], speed [64,81,82], horizontal and vertical position of the load [115,116], and load mass.

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