FORGESOLAR GLARE ANALYSIS

Project: Honey Creek Solar

Honey Creek Solar will include approximately 40 acres of agricultural land in the city of East Troy, WI. Some light grading and clearing may take place but there will be little change to the quantity of impervious surface. It is expected that the project will generate 6 MW of power.

Site configuration: Untitled

Created 04 Feb, 2025 Updated 04 Feb, 2025 Time-step 1 minute Timezone offset UTC-6 Minimum sun altitude 0.0 deg DNI peaks at 1,000.0 W/m² Category 5 MW to 10 MW Site ID 140568.23785

Ocular transmission coefficient 0.5 Pupil diameter 0.002 m Eye focal length 0.017 m Sun subtended angle 9.3 mrad PV analysis methodology V2



Summary of Results No glare predicted

PV Array	Tilt	Orient	Annual Gr	een Glare	Annual Ye	llow Glare	Energy
	0	0	min	hr	min	hr	kWh
PV array 1	SA tracking	SA tracking	0	0.0	0	0.0	18,570,000.0

Total glare received by each receptor; may include duplicate times of glare from multiple reflective surfaces.

Receptor	Annual Green Glare		Annual Yellow Glare		
	min	hr	min	hr	
OP 1	0	0.0	0	0.0	
OP 2	0	0.0	0	0.0	
OP 3	0	0.0	0	0.0	
OP 4	0	0.0	0	0.0	
OP 5	0	0.0	0	0.0	
OP 6	0	0.0	0	0.0	
OP 7	0	0.0	0	0.0	
OP 8	0	0.0	0	0.0	
OP 9	0	0.0	0	0.0	
OP 10	0	0.0	0	0.0	
OP 11	0	0.0	0	0.0	



Component Data

PV Arrays

Name: PV array 1

Axis tracking: Single-axis rotation Backtracking: Shade-slope Tracking axis orientation: 180.0° Max tracking angle: 52.0° Resting angle: 52.0° Ground Coverage Ratio: 0.3 Rated power: 6000.0 kW

Panel material: Light textured glass with AR coating

Reflectivity: Vary with sun

Slope error: correlate with material



Vertex	Latitude (°)	Longitude (°)	Ground elevation (ft)	Height above ground (ft)	Total elevation (ft)
1	42.792480	-88.502698	889.88	7.00	896.88
2	42.792433	-88.499179	908.17	7.00	915.17
3	42.786056	-88.499222	891.80	7.00	898.80
4	42.786103	-88.501303	874.46	7.00	881.46
5	42.786670	-88.501389	887.85	7.00	894.85
6	42.786937	-88.501089	890.53	7.00	897.53
7	42.787914	-88.501239	884.99	7.00	891.99
8	42.788087	-88.502827	882.59	7.00	889.59

Discrete Observation Point Receptors

Name	ID	Latitude (°)	Longitude (°)	Elevation (ft)	Height (ft)
OP 1	1	42.792811	-88.500510	900.69	5.50
OP 2	2	42.793205	-88.499565	909.35	10.00
OP 3	3	42.793583	-88.500531	903.62	17.50
OP 4	4	42.793236	-88.501990	886.46	10.00
OP 5	5	42.793646	-88.504608	900.73	17.50
OP 6	6	42.792685	-88.504072	906.08	17.50
OP 7	7	42.791425	-88.503599	900.70	17.50
OP 8	8	42.789599	-88.504587	904.19	17.50
OP 9	9	42.792039	-88.495639	912.01	5.50
OP 10	10	42.793598	-88.497978	914.23	17.50
OP 11	11	42.792370	-88.494888	908.74	17.50



Glare Analysis Results

Summary of Results No glare predicted

PV Array	Tilt	Orient	Annual Gr	een Glare	Annual Yel	low Glare	Energy
	0	0	min	hr	min	hr	kWh
PV array 1	SA tracking	SA tracking	0	0.0	0	0.0	18,570,000.0

Total glare received by each receptor; may include duplicate times of glare from multiple reflective surfaces.

Receptor	Annual Green Glare		Annual Yellow Glare		
	min	hr	min	hr	
OP 1	0	0.0	0	0.0	
OP 2	0	0.0	0	0.0	
OP 3	0	0.0	0	0.0	
OP 4	0	0.0	0	0.0	
OP 5	0	0.0	0	0.0	
OP 6	0	0.0	0	0.0	
OP 7	0	0.0	0	0.0	
OP 8	0	0.0	0	0.0	
OP 9	0	0.0	0	0.0	
OP 10	0	0.0	0	0.0	
OP 11	0	0.0	0	0.0	

PV: PV array 1 no glare found

Receptor results ordered by category of glare

Receptor	Annual Gro	Annual Green Glare		low Glare
	min	hr	min	hr
OP 1	0	0.0	0	0.0
OP 2	0	0.0	0	0.0
OP 3	0	0.0	0	0.0
OP 4	0	0.0	0	0.0
OP 5	0	0.0	0	0.0
OP 6	0	0.0	0	0.0
OP 7	0	0.0	0	0.0
OP 8	0	0.0	0	0.0
OP 9	0	0.0	0	0.0
OP 10	0	0.0	0	0.0
OP 11	0	0.0	0	0.0



PV array 1 and OP 1

No glare found

PV array 1 and OP 2

No glare found

PV array 1 and OP 3

No glare found

PV array 1 and OP 4

No glare found

PV array 1 and OP 5

No glare found

PV array 1 and OP 6

No glare found

PV array 1 and OP 7

No glare found

PV array 1 and OP 8

No glare found

PV array 1 and OP 9

No glare found

PV array 1 and OP 10

No glare found

PV array 1 and OP 11

No glare found



Assumptions

"Green" glare is glare with low potential to cause an after-image (flash blindness) when observed prior to a typical blink response time. "Yellow" glare is glare with potential to cause an after-image (flash blindness) when observed prior to a typical blink response time. Times associated with glare are denoted in Standard time. For Daylight Savings, add one hour.

The algorithm does not rigorously represent the detailed geometry of a system; detailed features such as gaps between modules, variable height of the PV array, and support structures may impact actual glare results. However, we have validated our models against several systems, including a PV array causing glare to the air-traffic control tower at Manchester-Boston Regional Airport and several sites in Albuquerque, and the tool accurately predicted the occurrence and intensity of glare at different times and days of the year.

Several V1 calculations utilize the PV array centroid, rather than the actual glare spot location, due to algorithm limitations. This may affect results for large PV footprints. Additional analyses of array sub-sections can provide additional information on expected glare. This primarily affects V1 analyses of path receptors.

Random number computations are utilized by various steps of the annual hazard analysis algorithm. Predicted minutes of glare can vary between runs as a result. This limitation primarily affects analyses of Observation Point receptors, including ATCTs. Note that the SGHAT/ ForgeSolar methodology has always relied on an analytical, qualitative approach to accurately determine the overall hazard (i.e. green vs. yellow) of expected glare on an annual basis.

The analysis does not automatically consider obstacles (either man-made or natural) between the observation points and the prescribed solar installation that may obstruct observed glare, such as trees, hills, buildings, etc.

The subtended source angle (glare spot size) is constrained by the PV array footprint size. Partitioning large arrays into smaller sections will reduce the maximum potential subtended angle, potentially impacting results if actual glare spots are larger than the sub-array size. Additional analyses of the combined area of adjacent sub-arrays can provide more information on potential glare hazards. (See previous point on related limitations.)

The variable direct normal irradiance (DNI) feature (if selected) scales the user-prescribed peak DNI using a typical clear-day irradiance profile. This profile has a lower DNI in the mornings and evenings and a maximum at solar noon. The scaling uses a clear-day irradiance profile based on a normalized time relative to sunrise, solar noon, and sunset, which are prescribed by a sun-position algorithm and the latitude and longitude obtained from Google maps. The actual DNI on any given day can be affected by cloud cover, atmospheric attenuation, and other environmental factors.

The ocular hazard predicted by the tool depends on a number of environmental, optical, and human factors, which can be uncertain. We provide input fields and typical ranges of values for these factors so that the user can vary these parameters to see if they have an impact on the results. The speed of SGHAT allows expedited sensitivity and parametric analyses.

The system output calculation is a DNI-based approximation that assumes clear, sunny skies year-round. It should not be used in place of more rigorous modeling methods.

Hazard zone boundaries shown in the Glare Hazard plot are an approximation and visual aid based on aggregated research data. Actual ocular impact outcomes encompass a continuous, not discrete, spectrum.

Glare locations displayed on receptor plots are approximate. Actual glare-spot locations may differ.

Refer to the Help page at www.forgesolar.com/help/ for assumptions and limitations not listed here.

Default glare analysis parameters and observer eye characteristics (for reference only):

Analysis time interval: 1 minute
Ocular transmission coefficient: 0.5
Pupil diameter: 0.002 meters

Eye focal length: 0.017 metersSun subtended angle: 9.3 milliradians

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