

Table 2.3.10 DESIGN DATA FOR HI-STORM UMAX VERSION MSE (Properties listed in Table 2.3.2 remain unchanged except for those listed below, item numbers from Table 2.3.2 used where applicable)			
No.	Type	Value (minimum or nominal, as applicable)	Comment
3.	Depth averaged density of subgrade in Space B (see Figure 2.4.4)	130 lb/ft ³	Required for shielding analysis and SSI analysis.
7.	Strain compatible effective shear wave velocity in Space B, V	344 ft/sec	A small value, computed using the site specific data at the San Onofre nuclear plant (documented in the Calculation Package [3.4.1]), used to magnify the inertial response of the system under the MSE.
10.	Design Basis Earthquake	Defined by Reg. Guide 1.60 spectra applied at the elevation of the Support Foundation Pad (SFP) (See Figures 2.4.5 and 2.4.6). The ZPAs of the two horizontal spectra, 1.5g's each, are vectorially combined to give the resultant ZPA of 2.12 g's. The vertical spectra is also Reg Guide 1.60 pegged at 1.0g.	Horizontal and vertical spectra shown in Figures 2.4.5 and 2.4.6 are based on 5% damping. Following the Newmark 100-40-40 response combination technique [2.6.7] endorsed by the Regulatory Guide 1.92 [2.4.7], the <i>resultant ZPA</i> for a 3-D earthquake site is defined as: $a_R = a_1 + 0.4a_2 + 0.4a_3$, where a_1 , a_2 and a_3 are the site's ZPAs in three orthogonal directions and $a_1 \geq a_2 \geq a_3$. Hence, the DBE <i>resultant ZPA</i> at the foundation surface elevations is 2.5 g's (=1.0×1.5g's + 0.4×1.5 g's + 0.4×1.0 g's) This Newmark resultant ZPA is cited as the limiting value authorized for HI-STORM UMAX CoC for Version MSE.
14.	Minimum compressive strength of SES in Space A (see Figure 2.4.4)	3,000 psi	Used in tornado missile impact analysis and SSI analysis

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